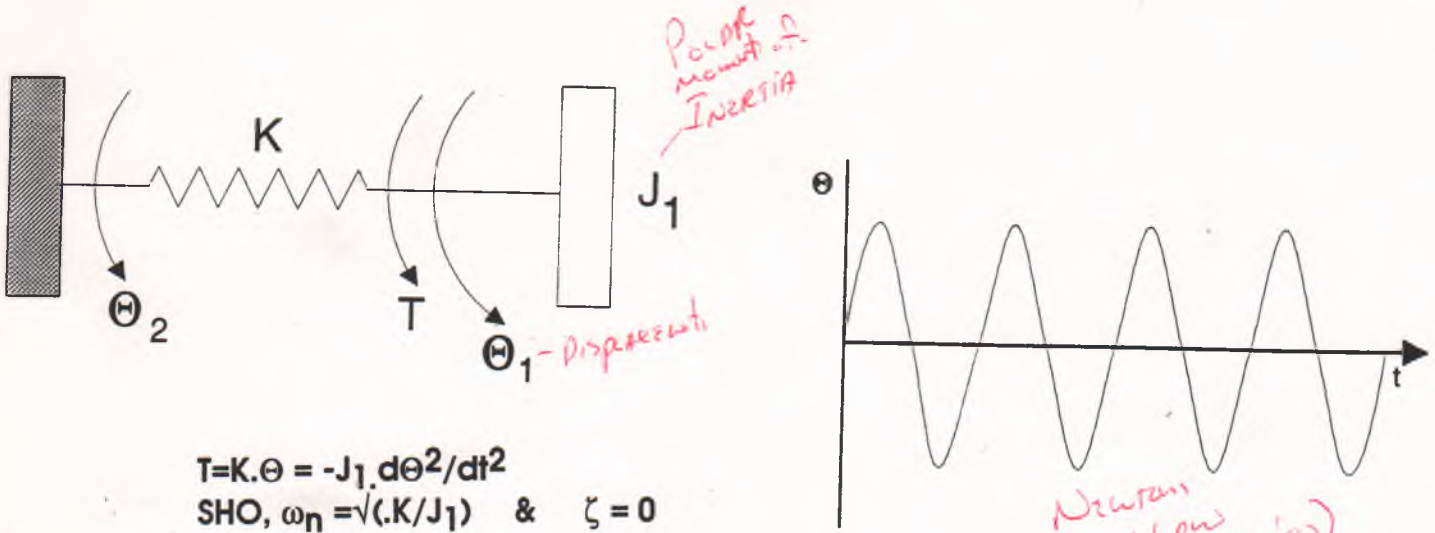
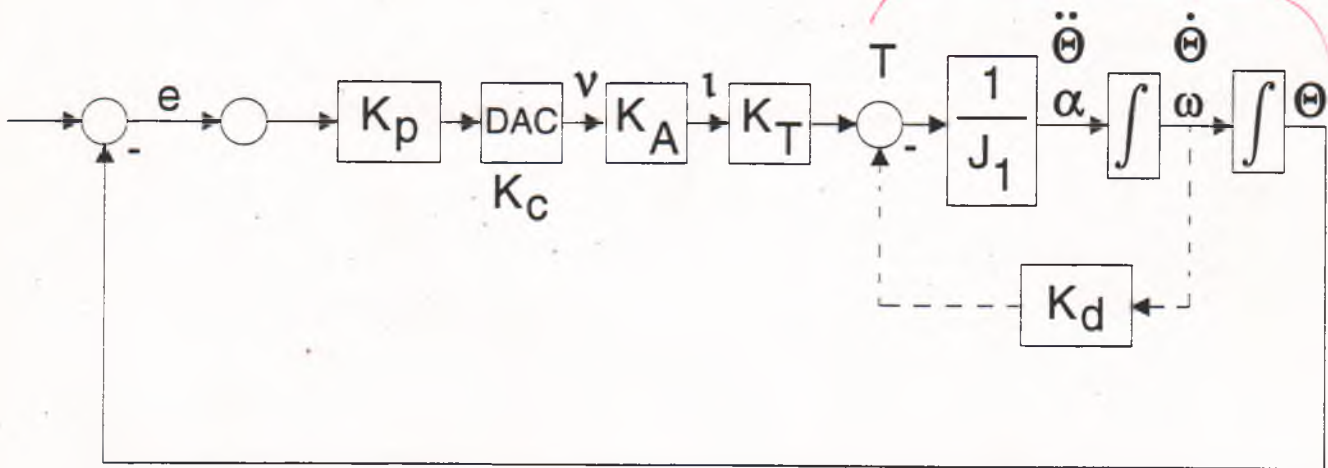


Proportional Control



$$T = K \cdot \theta = -J_1 \cdot d^2\theta / dt^2$$

$$\text{SHO, } \omega_n = \sqrt{(K/J_1)} \quad \& \quad \zeta = 0$$



Assuming small friction ($K_d = 0$),

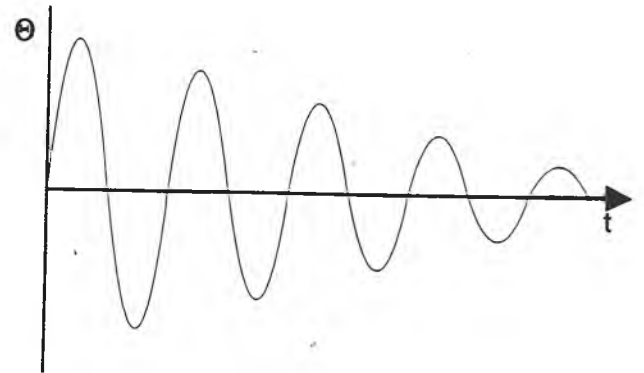
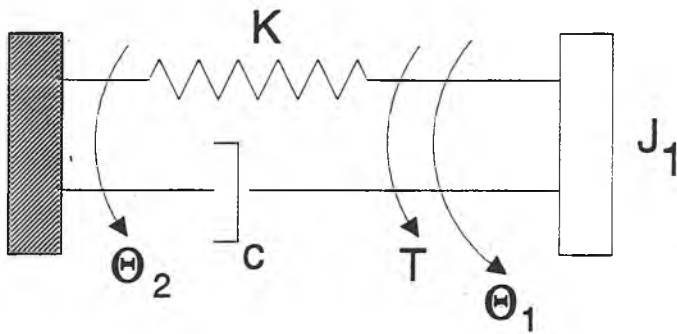
$$T(t) = K_p \cdot K_c \cdot K_A \cdot K_T \cdot e(t) = -K_p \cdot K_c \cdot K_A \cdot K_T \cdot \theta(t) = J_1 \cdot d^2\theta / dt^2$$

This is an undamped SHO.

$$\omega_n = \sqrt{((K_p \cdot K_c \cdot K_A \cdot K_T) / J_1)} \quad \& \quad \zeta = 0$$

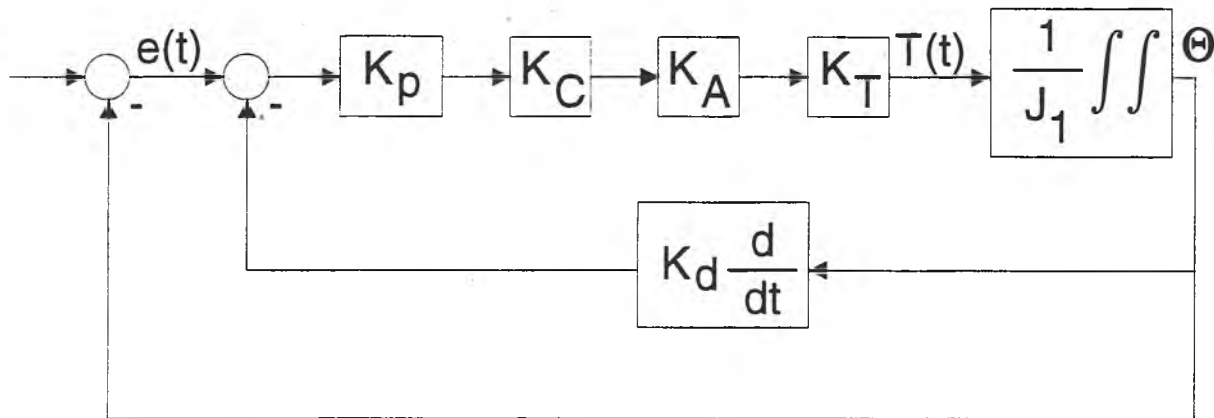
- Thus the proportional gain $K_p \rightarrow$ spring stiffness
- Higher $K_p \rightarrow$ higher Stiffness

Derivative Control



$$T = K \cdot \Theta + c \cdot \frac{d\Theta}{dt} = -J_1 \cdot \frac{d^2\Theta}{dt^2}$$

damped SHO, $\omega_n = \sqrt{(K/J_1)}$ & $\zeta = (c/2\sqrt{(k \cdot J_1)})$

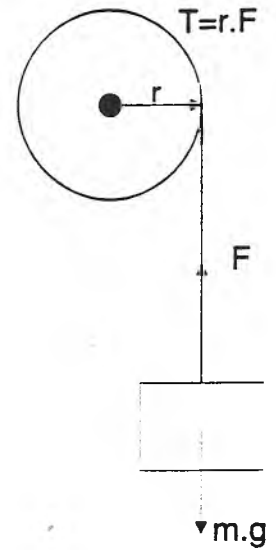


$$T(t) = -K_p \cdot K_c \cdot K_A \cdot K_T \cdot \Theta(t) - K_p \cdot K_c \cdot K_A \cdot K_T \cdot K_d \cdot \frac{d\Theta}{dt} = J_1 \cdot \frac{d^2\Theta}{dt^2}$$

This is a damped SHO,

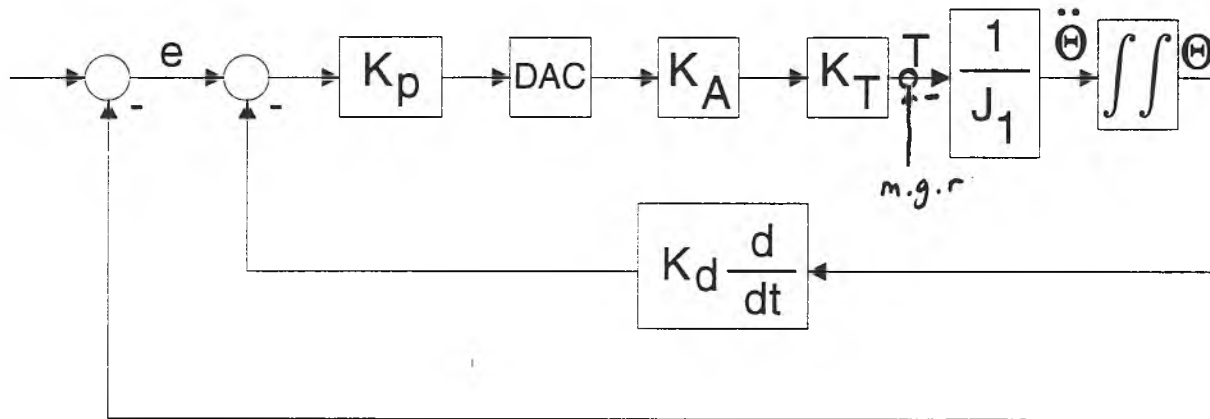
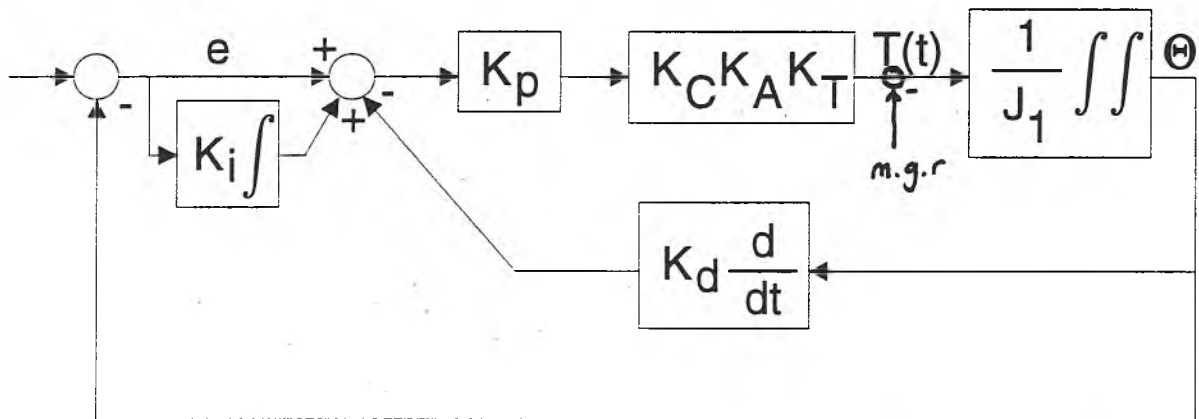
$$\omega_n = \sqrt{((K_p \cdot K_c \cdot K_A \cdot K_T) / J_1)} \quad \& \quad \zeta = (K_d / 2\sqrt{(J_1 / K_p \cdot K_A \cdot K_T \cdot K_c)})$$

Integral Term



Without Integral:

$$T(t) = K_p \cdot K_C \cdot K_A \cdot K_T \cdot e(t) = m \cdot g \cdot r$$



With Integral

$$T(t) = (K_p \cdot K_C \cdot K_A \cdot K_T) \cdot (K_i \int e(t) dt + e(t)) = m \cdot g \cdot r$$

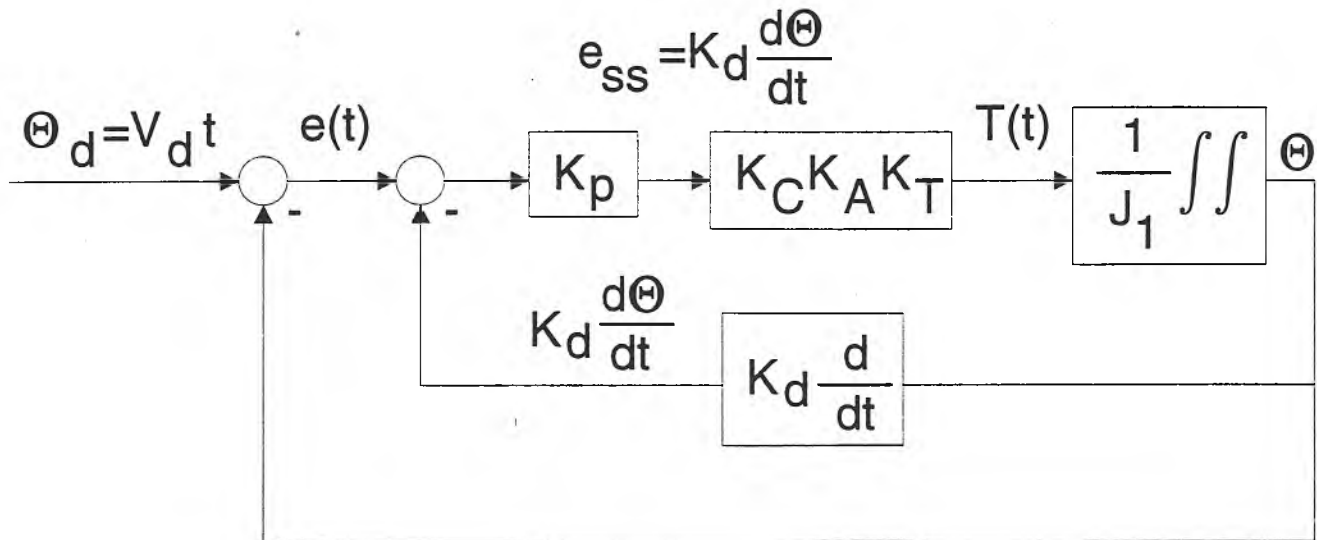
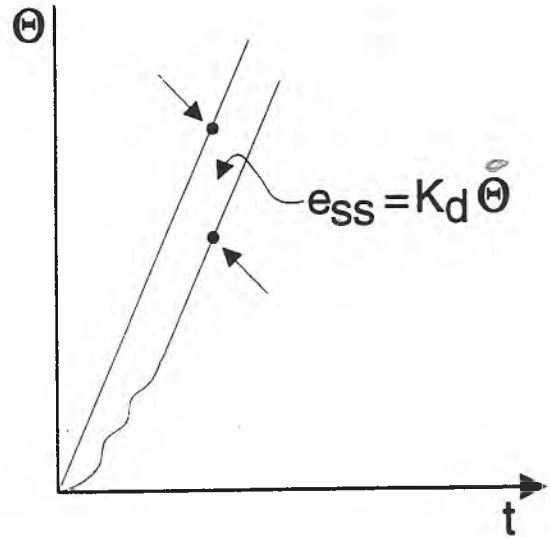
therefore as $t \rightarrow \infty$, $e(t) \rightarrow 0$

Errors at Steady State Due Constant Speed Trajectory Tracking

Ramp Input: $\Theta_d = V_d \cdot t$, $d\Theta/dt = V_d$, $d^2\Theta/dt^2 = 0$

Results (assuming friction ≈ 0):

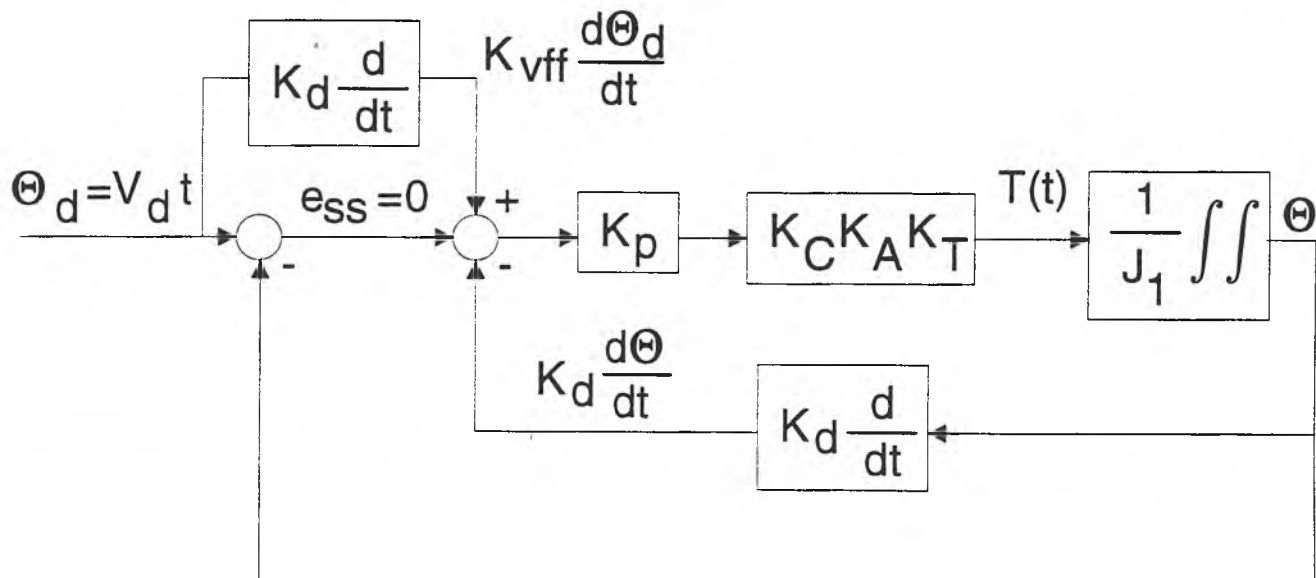
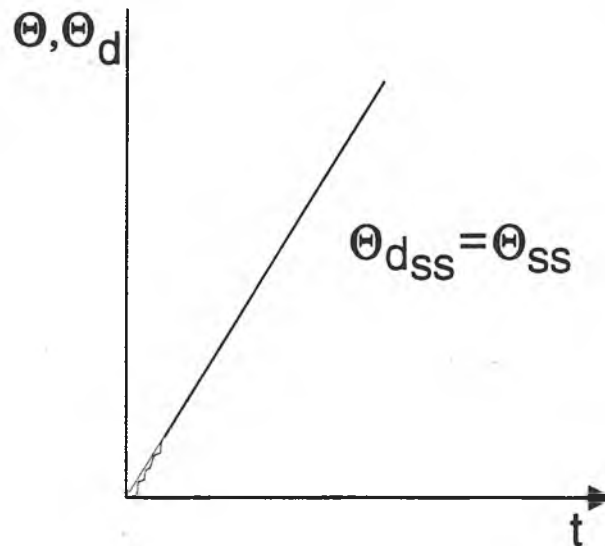
$$T_{ss} \approx e_{ss} - K_d \cdot d\Theta/dt = 0$$



Purpose of Velocity Feedforward

Selecting $K_{vff} = K_d \rightarrow e_{ss} = 0$

No *steady State* error due to constant velocity tracking.



Purpose of Acceleration Feedforward

In general, the trajectories contain higher order time functions:

e.g. : Constant jerk trajectory $\Theta_d(t) = c_0 + c_1.t + c_2.t^2$

By choosing,

$$K_{aff} = J_1 / (K_p \cdot K_C \cdot K_A \cdot K_T) \rightarrow e(t) = 0$$

This results in no tracking error for the *Ideal* system.

Since,

$$T(t) = (J_1 / (K_p \cdot K_C \cdot K_A \cdot K_T)) \cdot d^2\Theta_d/dt.^2 / (K_p \cdot K_C \cdot K_A \cdot K_T) = J_1 \cdot d^2\Theta_d/dt.^2$$

$$\rightarrow d^2\Theta_d/dt.^2 = d^2\Theta/dt.^2 \rightarrow \Theta_d(t) = \Theta(t) \rightarrow \text{No tracking errors}$$

